

## **Analysis of drying kinetic of brewer's spent grains: effect of the temperature on the physical properties and the content of bioactive compounds**

### **Análisis de la cinética de secado del bagazo residual de malta: efecto de la temperatura sobre las propiedades físicas y el contenido de compuestos bioactivos**

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#### **Abstract**

**Background:** Brewer's spent grain (BSG) is a biomass by-product generated in large volumes during industrial beer production. BSG has become a growing environmental problem, as most breweries discard it inappropriately, negatively impacting the environment. Alternatives for the exploitation of this by-product have consisted of elaborating food supplements for farm animals, obtaining biofuels, developing adsorbents, and obtaining substances for the food industry. However, the high moisture content in BSG (approximately 70%), poses a significant challenge in exploring various reuse alternatives. Therefore, the implementation of a pre-drying process becomes essential.

**Objective:** This study aimed to analyze the BSG drying kinetics at different temperatures and the effect of the drying temperature on the physical properties and the content of bioactive compounds.

**Methods:** BSG samples were dried at different temperatures (50, 60, 70, 80, 90, and 105°C) and analyzed for their moisture ratio, water activity, total polyphenol content (TPC), and DPPH (1,1-diphenyl-2-picrylhydrazil) radical scavenging activity. Also, four kinetics models were fitted to the drying data.

**Results:** It was determined that the effective diffusivity was between  $5.23 \times 10^{-10}$  (m<sup>2</sup>/s) and  $2.49 \times 10^{-09}$  (m<sup>2</sup>/s), and the value of the activation energy was 28.05 kJ/mol. In

addition, it was found that the content of phenolic compounds ( $1.27\pm 0.120$  mg gallic acid equivalents /g) and the DPPH radical scavenging activity ( $0.21\pm 0.015$  mg gallic acid equivalents /g) were not significantly affected by the variation in the drying temperatures studied.

**Conclusions:** From an operational point of view, the most suitable temperature for the drying process of BSG was  $105^{\circ}\text{C}$  since it would allow to reach shorter drying times, and the TPC was not affected markedly by the range of temperature studied.

**Keywords:** Brewer's spent grain, dry kinetics, diffusion, polyphenols, by-products valorization.

## Resumen

**Antecedentes:** El Bagazo residual de malta (BSG por sus siglas en inglés) es un subproducto biomásico generado en grandes volúmenes durante la producción industrial de cerveza. El BSG se ha convertido en un creciente problema para el medio ambiente, debido a que la mayoría de las cervecías descartan inapropiadamente este residuo generando un impacto negativo al ambiente. Las alternativas para el aprovechamiento de este subproducto han consistido especialmente en la elaboración de suplementos alimenticios para animales de granja, obtención de biocombustibles, desarrollo de adsorbentes y obtención de productos para la industria alimentaria. Sin embargo, el alto contenido de humedad ( $\sim 70\%$ ) del BSG representa un reto para el desarrollo de diferentes alternativas de reutilización, por lo que se hace necesario un proceso de secado previo.

**Objetivos:** En este estudio se analizó la cinética de secado del BSG a diferentes temperaturas y el efecto de la temperatura de secado sobre sus propiedades físicas y contenido de compuestos bioactivos.

**Métodos:** Las muestras de BSG fueron secadas a diferentes temperaturas ( $50, 60, 70, 80, 90$  y  $105^{\circ}\text{C}$ ) y analizadas en términos de razón de humedad, actividad acuosa, contenido de polifenoles totales (TPC) y actividad secuestradora del radical DPPH. Además, se ajustaron 4 modelos cinéticos a los datos de secado.

**Resultados:** Se determinó que la difusividad efectiva del BSG varió entre  $5.23\times 10^{-10}$  ( $\text{m}^2/\text{s}$ ) y  $2.49\times 10^{-09}$  ( $\text{m}^2/\text{s}$ ). El valor de la energía de activación fue de  $28.05$  kJ/mol. Además, se encontró que el contenido de compuestos fenólicos ( $1.27\pm 0.120$  mg equivalentes de ácido gálico/g) y la actividad secuestradora del radical DPPH ( $0.21\pm 0.015$  mg equivalentes de ácido gálico/g) no se vieron significativamente afectados por el rango de temperaturas estudiadas.

**Conclusiones:** Desde un punto de vista operativo, se determinó que la temperatura de secado más adecuada para el BSG fue de  $105^{\circ}\text{C}$ , debido a que permitió alcanzar tiempos de secado más cortos, y, además, el TPC no se vio significativamente afectado en el rango de temperaturas estudiadas.

**Palabras clave:** Bagazo residual de malta, cinética de secado, difusión, polifenoles, valorización de subproductos.

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## 1. Introduction

Within the alcohol industry, beer is the most consumed drink globally (1,2). Over time, the brewing process has undergone various transformations until it reaches the industrial production process that we generally know today (1,3,4). The process of obtaining the beer consists of the malting stage of the fermentable source (barley grain, rice grain, among others), grinding and maceration, obtaining the wort, refrigeration, and fermentation (5). A solid and wet by-product is obtained during maceration, known as Brewer's spent grain (BSG). BSG represents 85% of all solid by-products generated by beer production (4,6). World beer production for 2018 reached  $\sim 1940 \times 10^6$  hectolitres ( $194 \times 10^6 \text{ m}^3$ ) (6), of which  $\sim 582 \times 10^6$  hectolitres ( $\sim 30\%$  of world production) were produced in the Americas (7). The countries with the highest beer production for 2020 were China ( $\sim 341 \times 10^6$  hectolitres), the USA ( $\sim 212 \times 10^6$  hectolitres), and Brazil ( $\sim 152 \times 10^6$  hectolitres) (8). In Colombia, it is estimated that the annual production of beer is approximately  $22 \times 10^6$  hectolitres (8), considering that for every 100 liters of beer obtained, 20 kg of BSG are produced (6), the amount of bagasse generated is a little over  $440 \times 10^3$  Ton per year. These large volumes of by-products are becoming a growing environmental problem due to their unwillingness to discard them (4,6,7,9-11).

In recent years there has been growing scientific and political interest in the exploitation and valorization of residual biomass (12), such as BSG. It is partly due to the concept of circular bioeconomy has gained in the global economy (13,14). The circular bioeconomy consists of an environmentally and socially sustainable economy through biological resources production, use and reuse (15,16). Therefore, finding different alternatives for using residual biomass, such as BSG, is considered a current challenge for scientific research.

Searching for technological alternatives for the use of BSG has brought with it the development and application of different technologies, for example, a food supplement for farm animals based on BSG due to its rich protein content (17). Other studies have found that it can be used for energy production (18), obtaining biodiesel (19), and bioethanol (20). Other authors have investigated the use of BSG for various purposes, such as obtaining coenzymes, graphene for electrode production (21), activated carbons (22), and obtaining food products for human consumption (23), among others.

The BSG has a high moisture content ( $\sim 70-73\%$ ) (19,24,25); this makes it challenging to handle and store. In addition, higher moisture favors the presence of microorganisms that degrade biomass making it difficult to reuse and practical application for the options mentioned above. In line with reusing the BSG, it must be made a pre-drying treatment to improve its handling and storage conditions. Various drying techniques have been employed, including infrared, freeze drying, convective hot air drying, and solar drying. Among these methods, convective drying is the widely utilized approach in industrial settings for mass production (26-30). During the development of a laboratory-scale production process, it is crucial to consider upscaling it for industrial applications. Therefore, gaining a comprehensive understanding of drying kinetics becomes paramount, with theoretical and semi-theoretical models playing a pivotal role in this regard.

Semi-theoretical models are typically derived by simplifying the general series of Fick's second law or modifying existing simplified models (31). Empirical and semi-theoretical models have the advantage of requiring less computational time and do not necessitate complex assumptions about the geometry, mass diffusivity, and conductivity of the specific food product (31). These models have been widely used for modeling the drying

kinetics of agri-food products such as watermelon seeds, turnips, and coffee beans (26,29,32,33). In the literature, few kinetic studies of BSG drying are directed to find the best drying temperature and its influence on some characteristics such as water activity, intrinsic moisture of BSG drying, and the content of antioxidant compounds present in the extract obtained.

This work aimed to study a temperature range for the drying process of the BSG, favoring the operation time. For this purpose, drying kinetics were studied, and different kinetic models were applied to the experimental data to predict drying behavior. Fick's second law of mass transfer was used to determine effective diffusivity and activation energy. The change in moisture ratio, water activity, and color of the BSG after drying at different temperatures was also evaluated. Finally, the influence of the drying temperature on the content of phenolic compounds and the antioxidant activity present in the extract obtained from BSG was evaluated.

## **2. Materials and Methods**

### **2.1. Materials**

Brewer's spent grain (BSG) was supplied by a brewing company in the tacaoca desert (Huila, Colombia). The bagasse was frozen for storage and later use. Ethanol (70% v/v) and analytical grade sodium carbonate ( $\text{Na}_2\text{CO}_3$ ) (LOBA Chemie, India) were used. Folin-Ciocalteu reagent, gallic acid, and the 1,1-diphenyl-2-picrylhydrazil (DPPH) free radical were purchased from PanReac AppliChem (Spain).

### **2.2. Drying assays**

The drying process of the BSG was carried out on a convection oven (Memert UF 110, Memmert Universal, Schwabach, Germany) equipped with a temperature controller. The evaluated temperatures (50°C, 60°C, 70°C, 80°C, 90°C, and 105°C) were selected based on previous studies and practical considerations, aiming to cover a wide range of drying conditions commonly encountered in industrial and laboratory settings (26,29,33). The process consisted of weighing approximately 10 g of BSG in a Petri box, putting it into the oven, and drying it at the defined temperature. The variation in the sample weight was recorded at intervals; this procedure was repeated until constant weight, indicating that the equilibrium had been reached. The weight recorded up to equilibrium also allowed the sample to obtain moisture. Under the established conditions, it was assumed that the resistance to heat transfer within the particle and in the outer gaseous phase was negligible (33). The reported results corresponded to average values obtained from tests performed in triplicate at each temperature.

The moisture ratio was (MR) obtained by applying the following equation (Eq 1) (34):

$$MR = \frac{m_t - m_e}{m_i - m_e} \quad (1)$$

where  $m_t$  is the moisture content at time  $t$ , present in the BSG;  $m_i$  is the initial moisture content of the sample, and  $m_e$  is the moisture at the equilibrium over a long enough time to ensure constant weight. Four commonly used mathematical models were used to adjust the drying curve under isothermal conditions (31): Newton, Page, Logarithmic, and Midilli-Kucuk. The differences between the experimental and theoretical values given by each model were evaluated using the statistics of the adjusted coefficient of determination ( $R^2_a$ ), the standard deviation (SD), and the coefficient of variance (CV).

$$R^2_a = 1 - \left[ \frac{N-1}{N-p-1} * (1 - R^2) \right] \quad (2)$$

$$SD = \frac{\sqrt{\sum_{i=1}^N (MR_{exp} - MR_{mod})^2}}{N-1} \quad (3)$$

$$CV = \frac{SD}{\overline{MR_{exp}}} \quad (4)$$

where  $N$  is the number of experimental data;  $p$  is the number of model parameters;  $R^2$  is the coefficient of determination;  $MR_{exp}$  is the experimental moisture data;  $MR_{mod}$  is the theoretical moisture, and  $\overline{MR_{exp}}$  is the average of the experimental moisture data.

### 2.3. Determination of the effective diffusivity

The equation of the second law of Fick Eq (5) was used for effective diffusivity ( $D_{eff}$ ) determination. This equation describes the diffusion of water during the drying process, where the resistance to mass transfer that limits the drying speed is given by internal resistance, that is, the transfer of water from inside the BSG to the surface (35,36).

$$\frac{\partial MR}{\partial t} = \nabla [D_{eff} (\nabla MR)] \quad (5)$$

One of the analytical solutions of the second law of Fick for flat geometries, long drying periods and values of  $MR < 0.6$  is presented in Eq (6) (37).

$$MR = \frac{8}{\pi^2} - \exp\left(\frac{\pi^2 D_{eff}}{L^2} t\right) \quad (6)$$

where  $D_{eff}$  is the effective diffusivity ( $m^2/s$ ),  $L$  is the characteristic length (m), and  $t$  is the drying time (s). Characteristic length  $L$  was determined using Eq. (7), considering the mass of the sample  $W$ , the density  $\rho$ , and the cross-sectional area of the sample  $A_t$ .

$$L = \frac{W}{\rho A_t} \quad (7)$$

It is known that effective diffusivity can commonly be determined by graphing the experimental data linearizing Eq. (6) as shown in Eq (8).

$$\ln(MR) = \ln \frac{8}{\pi^2} - \left(\frac{\pi^2 D_{eff}}{L^2}\right) t \quad (8)$$

After plotting  $\ln(MR)$  vs.  $t$ , the  $D_{eff}$  value was obtained from the slope of equation Ec (8). For calculating the activation energy  $E_o$  an expression of Arrhenius was used (19,34) Eq. (9), which relates effective diffusivity, temperature, and activation energy. Where  $D_o$  is the pre-exponential factor;  $T$  is the absolute temperature; and  $R$  is the general constant of the gases.

$$D_{eff} = D_o \exp\left(\frac{-E_o}{RT}\right) \quad (9)$$

## 2.4. Moisture and water activity.

For intrinsic moisture determination, approximately 0.5g of dry and ground BSG was weighed in a moisture balance (Citizen MB-50 Moisture Analyser Balance, Japón). The water activity was determined in a water activity analyzer equipment (AquaLab PRE, USA), the sample was entered, and the value determined by the equipment was recorded. All measurements were made in triplicate for each BSG sample dried at the studied temperatures. The recorded value corresponds to the average value of the measurements.

## 2.5. Color

The color of the dry samples was measured using a tristimulus Minolta colorimeter (Konica-Minolta CR-10, Osaka, Japan) and reported in CIELab parameters ( $L^*$ ,  $a^*$  and  $b^*$  values), where  $L^*$  was used to denote lightness,  $a^*$  redness and greenness, and  $b^*$  yellowness and blueness (38). The equipment was calibrated using a white plate as standard. BSG samples were placed on this white plate, and the values of the parameter's "L", "a" and "b" were recorded. The total color difference ( $\Delta E$ ) was calculated using equation Eq (10).

$$\Delta E = \sqrt{(L - L^*)^2 + (a - a^*)^2 + (b - b^*)^2} \quad (10)$$

## 2.6. Determination of the content of bioactive compounds

Samples (1 g) of BSG were placed in 15 mL test tubes and mixed with 6 mL of 70 %v/v ethanol. Then, the tubes were immersed in an ultrasound bath (BRANSON model 1800, Germany) with a rectangular chamber (longe:10 cm, hight:12 cm, depth: 12cm) equipped with an industrial transducer operating at 40 kHz. A flow system (in/out) controlled the water temperature from a heating bath (Memmert WNB14, Germany), maintaining a constant temperature of 60 °C for 10 minutes. The extracts obtained were filtered (Double ring qualitative filter paper, grade: EXP DRQLM) and centrifuged at 5300  $m/s^2$  (4000 rpm) for 10 min. The extracts were suspended in water for all determinations at a dilution

factor of 9. This test was carried out in triplicate for each dried BSG sample at the studied temperatures.

### **2.6.1. Estimation of total polyphenols content**

The total polyphenols content (TPC) of BSG was determined by the Folin-Ciocalteu method <sup>(39)</sup>. Briefly, 400  $\mu$ L of each extract were mixed with 2 mL of 1:10 diluted Folin-Ciocalteu reagent. The mixtures were stirred for 30 s using a vortex mixer (Benchmark, USA), and then 160  $\mu$ L of sodium carbonate (7% w/v) were added. After 30 min, the absorbance of the samples was measured at 760 nm using a spectrophotometer (X-ma 1200 Human Corporation, Loughborough, UK). Gallic acid was used as standard. The total polyphenols content was expressed as gallic acid equivalents (GAE) per gram of BSG.

### **2.6.2 Estimation of the DPPH•–scavenging activity**

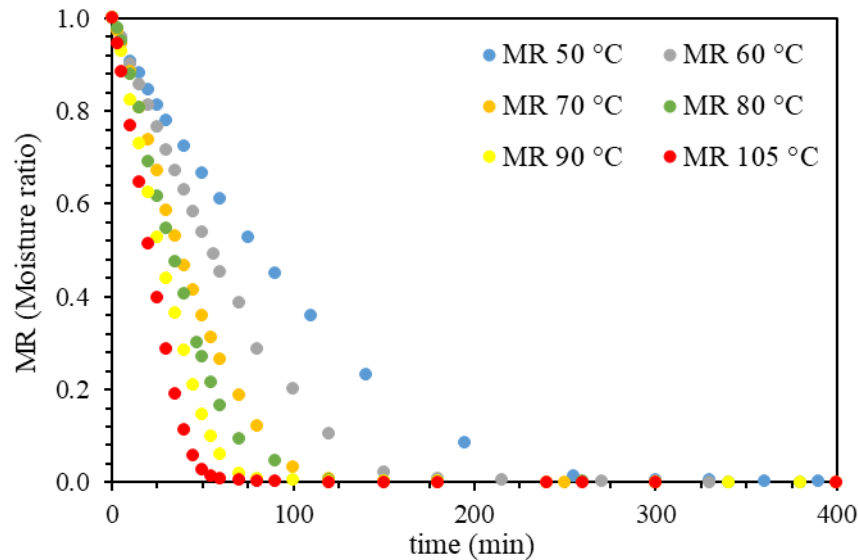
DPPH radical scavenging activity was tested as described Brand-Williams *et al.* (1995) <sup>(40)</sup>. A volume of 100  $\mu$ L of each obtained extract was mixed with 3,9 mL of an ethanolic solution of DPPH• (25 ppm). It was then vortexed for 30 s and kept in the dark for 30 min. Finally, the absorbance was measured at 517 nm using the spectrophotometer. Gallic acid was also used as standard, and the results were expressed as mg gallic acid per gram BSG (mg GAE/g BSG).

## **3.Results and discussions**

### **3.1. Drying kinetics analysis**

Figure 1 shows the drying curves of Brewer's spent grain (BSG) obtained at the different studied temperatures (50°C, 60°C, 70°C, 80°C, 90°C, and 105°C). It was observed that when the temperature increases, the curve's slope becomes greater, indicating that the humidity of the BSG reaches equilibrium or reaches a specific moisture ratio in shorter times. The equilibrium time is defined as the moment when sample mass does not vary in time; according to this, for the dried sample at 105°C, the equilibrium time was reached at 60 min, while at 50 °C, the equilibrium time took 260 min, four times more than observed at 105 °C. Recent studies on the drying kinetics of biomass corroborate the influence of temperature on the drying process. For instance, Ghanem *et. al.* found that increasing the drying temperature from 50 to 70 °C reduced the drying time by 30 % <sup>(41)</sup>. Similarly, another study reported that temperature is a critical factor for the drying kinetics of sawdust, affecting the drying process <sup>(42)</sup>. Additionally, the literature suggests that the drying kinetics of biomass are affected by various parameters, including the type

and size of biomass, airflow rate, and moisture ratio. For example, a study by <sup>(43)</sup> examined the drying kinetics of palm kernel shells and determined that airflow rate and particle size significantly affect the drying process. From these curves presented in Figure 1, it was also determined that the initial humidity of BSG was 71.7 % ( $\pm 0.012$ ). This moisture ratio aligns with others reported in the literature <sup>(37,44)</sup>.

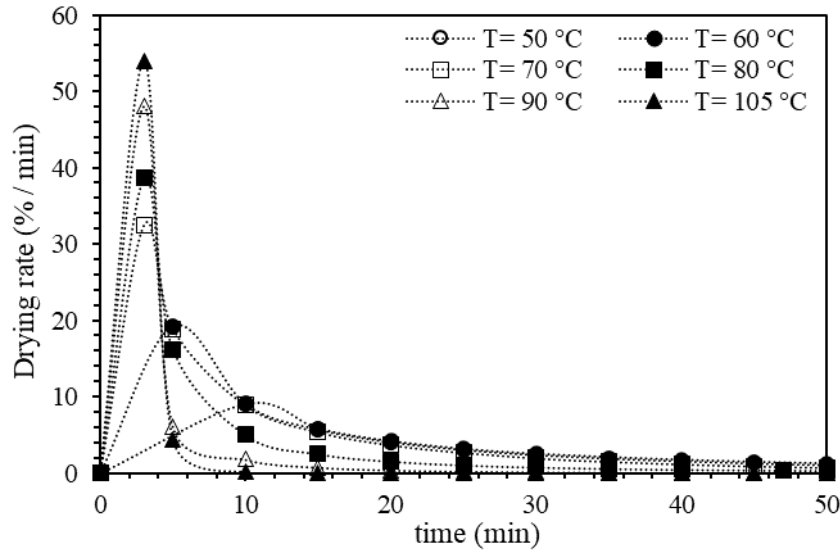


**Figure 1. Drying curves of Brewer's spent grain (BSG) using the different temperatures studied (experimental points).**

The drying speed curves of BSG obtained at the different studied temperatures are shown in Figure 2. It was observed that as the temperature increased, the slope of the curve was higher, indicating an increase in the drying speed. Besides, at the beginning of the curve, the positive slope indicated a short period where the drying speed increased. This increase corresponded to the period when the temperature inside the oven raised, promoting the evaporation process of the water from the particles' surface. It should be noted that this period became shorter as the temperature studied increased. Similar observation has been reported in previous studies on the effect of temperature on the drying rate of biomass <sup>(45)</sup>. A progressive decay of the drying rate was observed because the moisture on the surface of the particles was completely evaporated, while the remaining water within the BSG matrix evaporated slower. This behavior indicated that the internal resistance limits the drying speed to mass transfer, that is the diffusion of moisture from inside the BSG to its surface. Similar drying mechanism have been observed in other studies <sup>(19, 31, 33, 37, 46)</sup>. These findings were consistent with other studies on the drying kinetics of bamboo sawdust reported, the drying rate augmented with increasing temperature, and the drying process can be divided into three stages: the initial increasing rate period, the constant rate period, and the falling rate period, which was consistent with the observations made in this <sup>(47, 48)</sup>.

Figures 1 and 2 show that the drying speed was not constant in any of the conditions studied, probably because the thickness of the moisture layer, the "thin layer" on the surface, was not constant, preventing a continuous supply of moisture during the drying process. This behavior has also been observed in other studies <sup>(31, 46, 48)</sup>.





**Figure 2. Drying speed curves of Brewer's spent grain (BSG) at the different temperatures studied.**

The BSG drying curve was also evaluated using different masses; for this purpose, 105°C was used as the drying temperature because the process was performed faster. Figure S1 describes the drying curves at 105°C using different masses of BSG; it can be seen that the slope of the curve increased as the mass of BSG to be dried decreased. Also, the humidity to reach balance took 50, 60, and 80 min for 5g, 10g, and 15g, respectively. Therefore, the drying process took longer when there was more bagasse mass. This result corroborated that the internal resistance to mass transfer by the diffusion of moisture from the inside BSG particle to its surface was the limiting drying speed, as mentioned above, which is a common limiting factor in the drying kinetics of biomass. However, it is important to note that the drying kinetics of diverse types of biomasses may be influenced by various factors such as temperature, relative humidity, and particle size (30, 47, 48). Therefore, a comprehensive understanding of the drying behavior of each type of biomass is necessary to optimize the drying process for industrial applications.

### **3.2. Analysis of the effective diffusivity and of the activation energy of the drying process.**

Assuming that the sample throughout the drying process presented a negligible shrinkage, uniform distribution, and a constant content of initial moisture throughout the BSG particle, one of Fick's second law solutions was used to determine effective diffusivity. Figure S2 shows the graphs of  $\ln(\text{moisture ratio (MR)})$  vs.  $t$  (min), using equation Eq (8) and using the slope of each line was determined the effective diffusivity in each temperature studied.

Table 1 shows the values of effective diffusivity at different temperatures. Since  $D_{eff}$  was influenced by temperature, pressure, and molecular weight, the pressure, and molecular weight was assigned a constant value for this drying study. The increasing temperature and the effective diffusivity were greater because the higher the temperature increased the energy necessary for the water particles to begin the diffusion through the internal

structure of the BSG (Table 1).  $D_{eff}$  values in this analysis were in the order of magnitude found for other biomasses studies using BSG (33, 37). However, other recent studies have reported different results. For example, a study on the drying kinetics of corn stover reported that the effective diffusivity decreased with increasing temperature due to the formation of a crust layer on the biomass surface, which hindered moisture transfer (49, 50). These discrepancies highlight the importance of studying the specific characteristics of each type of biomass and the potential formation of crust layers during the drying process, as well as the need for further research to optimize drying conditions and reduce energy consumption in biomass drying processes.

**Table 1. Effective diffusivity at different temperatures and constant pressure (101.325 kPa)**

Temperature (°C)	50	60	70	80	90	105
Effective diffusivity (m <sup>2</sup> /s)	5.23x10 <sup>-10</sup>	8.22x10 <sup>-10</sup>	1.29x10 <sup>-09</sup>	1.39x10 <sup>-09</sup>	1.91x10 <sup>-09</sup>	2.49x10 <sup>-09</sup>

For the biomass drying process, such as BSG, the activation energy can be defined as the energy necessary for water particles to begin to diffuse through the solid structure of the BSG to the surface, and the drying process occurs (32, 51). For Activation Energy determination  $E_o$  (kJ/mol), the  $D_{eff}$  values recorded at the different temperatures were used; for this purpose, the  $\ln(D_{eff})$  vs.  $1/T$  was plotted (Figure S3). The results showed  $E_o$  values of around 28.05 kJ/mol. The pre-exponential coefficient  $D_o$  with a value of  $2.04 \times 10^{-5}$  m<sup>2</sup>/s was also determined. Activation energy has been widely used to analyze the drying kinetics of various types of biomasses, such as stevia leaves (52), tea (53), fructus aurantii (dried fruit of *Citrus aurantium* L.) (54), pomegranate arils (55), wood (56). These studies have reported activation energy values ranging from 13.5 kJ/mol for tea to 41.5 kJ/mol for wood, indicating that different types of biomasses have different activation energies due to variations in their internal structure and composition. In contrast, the  $E_o$  value obtained in this study for BSG was 28.05 kJ/mol, which is relatively low compared to other biomass studies. This difference in  $E_o$  values between BSG and other biomass is due to the unique structure and composition of BSG.

### 3.3. Analysis of the kinetic models

For kinetics analysis, four mathematical models were used to fit the experimental data: the model of Newton, Page, Logarithmic, and Midilli-Kucuk. With these models, it was desired to obtain the most suitable equation to estimate the moisture ratio (MR) of bagasse drying at different temperatures. Kinetic models are represented by the following Eq. (11-14):

$$\text{Newton model} \quad :MR = \exp(-Kt) \quad (11)$$

$$\text{Page model} \quad :MR = \exp(-Kt^n) \quad (12)$$

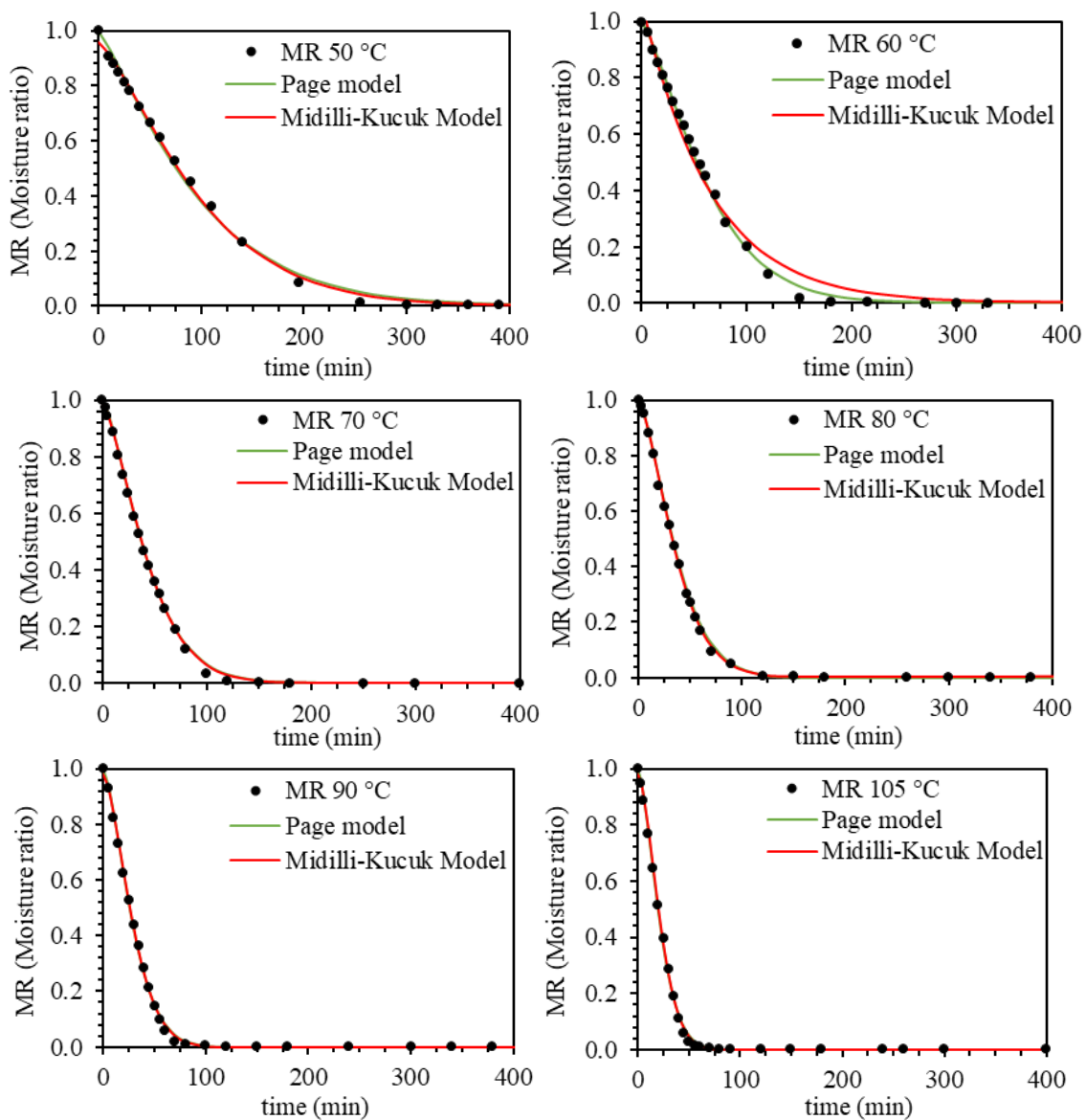
$$\text{Logarithmic model} \quad :MR = a + b \exp(-Kt) \quad (13)$$

$$\text{Midilli-Kucuk model} \quad :MR = a \exp(-Kt^n) + bt \quad (14)$$

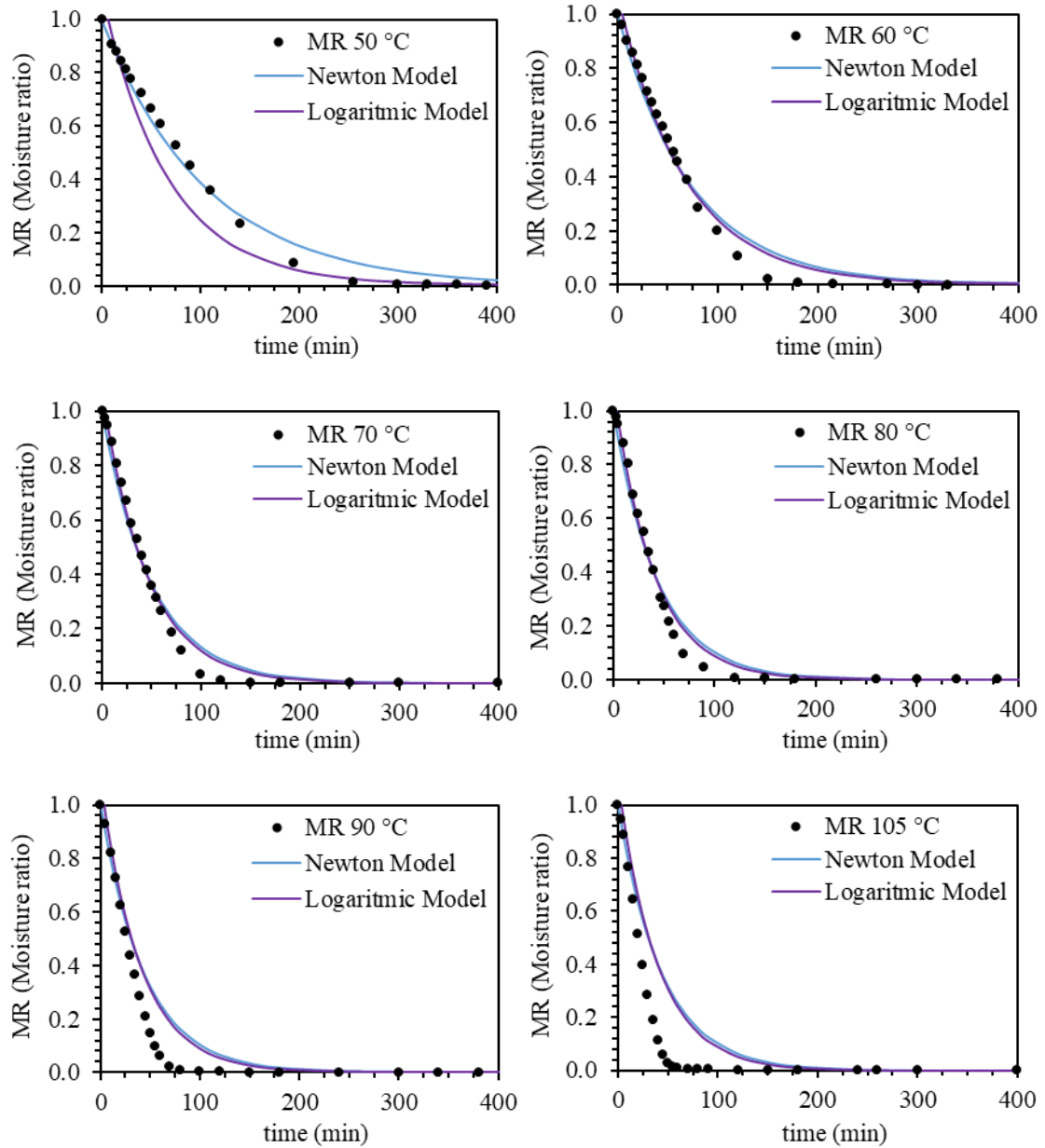
where  $K$  is the kinetic constant of each model,  $n$  is a power constant,  $a$  and  $b$  are parameters of the corresponding equation.

Figures 3 and 4 show the different models adjusted to the experimental data to facilitate the graphical analysis. The figures were grouped between the best-adjusted models (Figure 3) and those with more significant deviation (Figure 4).

Figure 3 shows the kinetic models that best fit the experimental data, the Page and Midilli-Kucuk models. In part, this is because the Midilli-Kucuk model contains a greater number of parameters with respect to the Page model; it was found that an equation with two parameters allows to adequately describe the drying kinetics of the BSG, in addition to being used to estimate the moisture ratio. Figure 4 shows the two kinetic models that had greater deviation when adjusting to the experimental data, Newton and the Logarithmic; observing that despite not adjusting as well as the Page and Midilli-Kucuk models, they could be used cautiously to have an estimated value of moisture during the drying process.



**Figure 3. Page and Midilli-Kucuk kinetic models adjusted to experimental drying curve data at different temperatures (50 °C, 60 °C, 70 °C, 80 °C, 90 °C, and 105 °C).**



**Figure 4. Newton and logarithmic kinetic models adjusted to experimental drying curve data at different temperatures (50 °C, 60 °C, 70 °C, 80 °C, 90 °C, and 105 °C).**

Table 2 presents the parameters of the different kinetic models adjusted to the experimental data. All parameter values from the kinetic models used are in the order of those found in the literature (29, 33, 51). The Page model was the one that best fit the experimental data; this can be deduced because this model obtained the values of  $R^2$  higher, lower  $SD$ , lower  $CV$ , and better graphic fit (Figure 3, Table 2). This model

contains relevant information to drying kinetics from the two parameters that fit the Page equation. The kinetic constant  $K$  and  $n$  grew slightly as the drying temperature increased. The growth of  $K$  was in line with the above results; as the temperature increased, the slope became larger. From the above, we concluded that a kinetic model with two parameters was sufficient to describe the drying kinetics of BSG adequately. The Page model allowed to have a robust model for predicting the drying kinetics of the precursor without the need to use a more complex equation using a greater number of parameters.

**Table 2. Kinetics models parameters**

Model	Temperature	Parameters				Statistics		
	(°C)	<i>a</i>	<i>B</i>	<i>n</i>	<i>K</i> ( <i>s<sup>n</sup></i> )	<i>r</i> <sup>2</sup>	<i>SD</i>	<i>CV</i>
Newton	50	-	-	-	0.009 4	0.989 7	0.03 8	0.08 5
	60	-	-	-	0.013 7	0.979 1	0.05 0	0.11 0
	70	-	-	-	0.020 1	0.972 4	0.05 5	0.11 2
	80	-	-	-	0.022 9	0.971 0	0.06 0	0.14 2
	90	-	-	-	0.022 9	0.896 4	0.10 8	0.34 4
	105	-	-	-	0.022 9	0.734 7	0.06 5	0.22 2
Page	50	-	-	1.2024	0.003 8	0.996 8	0.02 1	0.04 6
	60	-	-	1.3462	0.003 3	0.997 6	0.01 6	0.03 6
	70	-	-	1.3870	0.004 6	0.998 5	0.01 2	0.02 5
	80	-	-	1.4586	0.004 2	0.998 3	0.01 4	0.03 3
	90	-	-	1.5158	0.004 9	0.997 8	0.01 5	0.04 8
	105	-	-	1.5728	0.006 3	0.997 5	0.01 7	0.05 7
Logarítmi co	50	1.00E -03	1.100 0	-	0.015 0	0.928 1	0.09 5	0.21 3
	60	3.00E -07	1.068 7	-	0.015 0	0.983 8	0.04 2	0.09 2
	70	6.00E -07	1.072 1	-	0.021 9	0.979 2	0.04 5	0.09 1
	80	3.00E -07	1.086 3	-	0.025 2	0.977 4	0.04 8	0.11 4
	90	6.00E -07	1.086 3	-	0.025 2	0.890 6	0.10 2	0.32 6
	105	5.00E -07	1.086 3	-	0.025 2	0.695 1	0.05 6	0.19 0

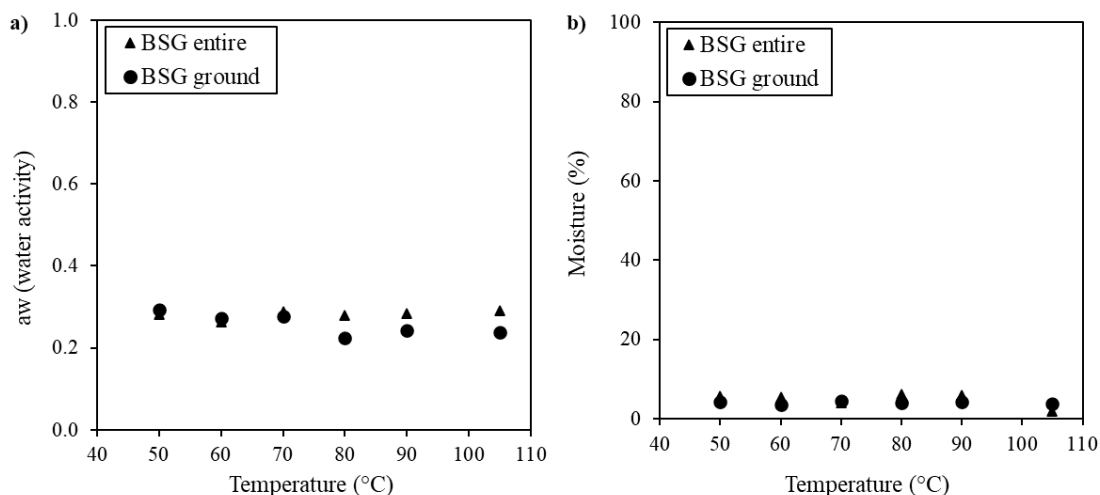
<b>Midilli-Kucuk</b>	50	0.958 3	0.00E +00	1.3223	0.002 1	0.997 6	0.01 6	0.03 6
	60	1.069 1	5.00E -07	1.0246	0.013 7	0.984 7	0.03 9	0.08 7
	70	0.986 3	6.00E -07	1.4262	0.003 9	0.998 5	0.01 1	0.02 3
	80	0.993 4	6.00E -06	1.5006	0.003 7	0.999 0	0.01 0	0.02 3
	90	0.978 6	4.00E -07	1.5753	0.003 9	0.997 8	0.01 4	0.04 4
	105	0.971 1	5.00E -07	1.6678	0.004 4	0.997 9	0.01 4	0.04 8

Figure S4 shows the kinetic models adjusted to the drying curves at a temperature of 105 °C using different masses of BSG. The parameters of the kinetic models were reported in Table S1. From Figure S4 and Table S1, the Page and Midilli-Kucuk models presented the best adjustments to the experimental data. In contrast, the Newton and Logarithmic models presented the greatest deviation. This behavior was similar to those illustrated in Figures 3 and 4.

### 3.4. Analysis of moisture and water activity

The effect of drying temperature on moisture content, water activity, and color of BSG after drying was analyzed. In addition, it was explored whether the BSG milling process affected the characteristics mentioned above after the drying process. These characteristics were compared in dry and whole BSG with dry and ground BSG.

Figure 5 shows the behavior of the water activity ( $a_w$ ) and the moisture of BSG as a function of the drying temperature. It was observed that the moisture and the water activity of BSG did not vary significantly, regardless of the temperature used in the drying. Besides, the whole and ground BSG samples showed moisture values of around 4.8% ( $\pm 1.614$ ) and 4.0% ( $\pm 0.366$ ), respectively, while similar  $a_w$  values were obtained for both samples ( $a_w \sim 0.26-0.28$ ) (Figure 5a). This result is an advantage from an application point of view since a material with low water activity and low moisture could stay longer in storage without affecting its shelf life, reducing the deterioration risk of BSG.



**Figure 5. Behavior of the water activity (a), and the moisture content (b) of the BSG samples as a function of drying temperature. These properties were measured for entire BSG and ground BSG.**

### 3.5. Color

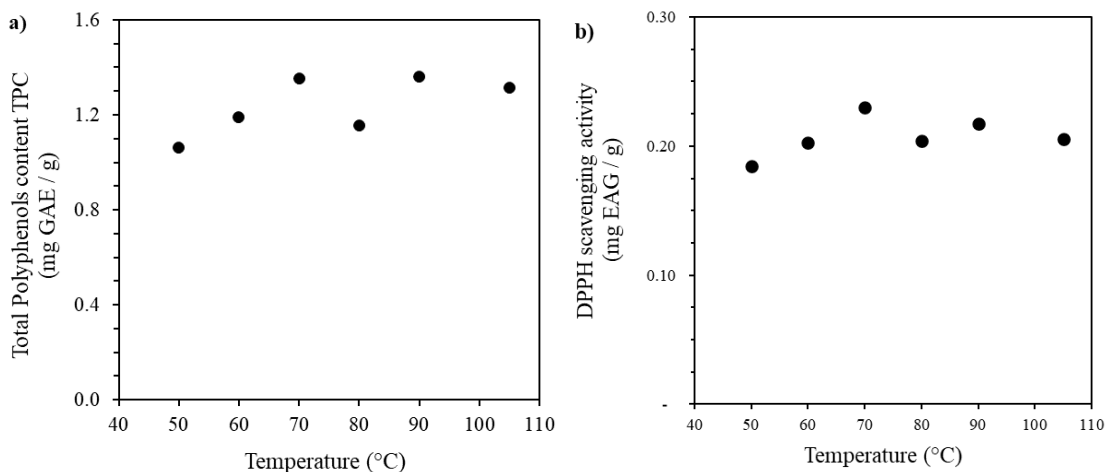
Figure S5 shows images of the whole and ground BSG samples, while the corresponding  $\Delta E$  values are shown in Table S2. It was observed that the different temperatures studied did not cause significant changes in the appearance of the samples nor in their color attributes. This behavior was probably due to the relatively low temperatures used, which were insufficient to alter the pigments present in both whole and ground BSG. Some studies reported that high drying temperatures can lead to a decrease in brightness and chroma of biomass samples, indicating a color change (53, 54, 57, 58). Therefore, it could be suggested that the effect of drying temperature on color stability varies depending on the specific type of biomass and the drying conditions used.

### 3.6. Analysis of the total phenolic content and DPPH radical scavenging activity

Figure 6 shows the behavior of the total polyphenol content and the DPPH radical scavenging activity of the BSG samples as a function of drying temperature.

The different drying temperature studied did not significantly influence the TPC (Figure 6a) or the DPPH radical scavenging activity (Figure 6b). The average phenolic content and DPPH scavenging activity were  $1.27 \pm 0.120$  mg GAE/g BSG and  $0.21 \pm 0.015$  mg GAE/g BSG, respectively. Yan et al. reported that the drying temperature had an impact on TPC and DPPH radical scavenging activity in both hot-air-dried and sunlight-dried orange black tea. Specifically, an increase in the drying temperature of orange black tea led to a decrease in TPC and antioxidant activity of the extract, with a more pronounced effect when hot-air was used as the drying method (53). Conversely, a previous study on microwave drying of lemon peel demonstrated an increased TPC when the applied power

was augmented. This behavior was attributed to the generation of high vapor pressure and temperature inside the plant tissue caused by the intense heat produced by microwaves, leading to the disruption of plant cell wall polymers. As a result, bound or cell wall phenolics may be released, potentially resulting in an increased extraction of phenolic compounds (41).



**Figure 6. Behavior of the total polyphenols content (a), and the DPPH radical scavenging activity (b) of the BSG samples as a function of drying temperature.**

## 4. Conclusions

Drying kinetics of Brewer's spent grain at different temperatures (50 °C, 60 °C, 70 °C, 80 °C, 90 °C, and 105 °C), and the effect of the drying temperature on the physical properties and the content of bioactive compounds were studied. It was observed that the internal diffusion of moisture limited the drying speed; the internal resistance is the governing mechanism for moisture transfer. The effective diffusivity values determined ranged from  $5.23 \times 10^{-10}$  (m<sup>2</sup>/s) to  $2.49 \times 10^{-9}$  (m<sup>2</sup>/s), and the activation energy value was 28.05 kJ/mol. The Page and Midilli-Kucuk models showed the best fit for the experimental data. In particular, a kinetic model with two parameters, such as the Page model, was sufficient to adequately describe the drying kinetics of BSG without the need to use a more complex equation using a greater number of parameters. Regardless of the drying temperature, the obtained BSG presented a low water activity and low intrinsic humidity that favors, in principle, greater storage and conservation times. It could be observed that the total phenolic content of  $1.27 (\pm 0.120)$  mg EAG/g BSG and DPPH radical scavenging activity  $0.21 (\pm 0.015)$  mg EAG/g BSG, present in the extract obtained from BSG, was not affected by temperature variation in the studied range. Therefore, phenolic compounds have antioxidant properties and can be used as animal food supplements. From an operational point of view, it is possible to conclude that the most suitable temperature for the drying process of BSG was 105 °C since it allowed shorter drying times. The latter would result in lower energy and operating costs. Studies are recommended to extract polyphenols utilizing Ultrasound-assisted extraction (UAE) on



a larger scale (pilot or industrial) to determine the feasibility of reusing BSG as a source of antioxidant substances by evaluating economic aspects, energy, and operations.

Conflicts of Interest: The authors declare no conflict of interest.

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